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: FEM Simulation of Machining AISI 1045 Steel Using Driven Rotary Tool

Penulis

1. Yanuar Burhanuddin

(NIP. 19640506 200003 100 1)

2. Suryadiwansa Harun

(NIP. 19700501 200003 100 1)

3. Gusri Akhyar Ibrahim

(NIP. 19710817 199802 100 3)

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Universitas Lampung

Penulis Utama,

Prof. Drs. Suharno, M.Sc., Ph.D

NIP. 196207171987031002

Dr. Yanuar Burhanuddin

NIP. 196405062000031001

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Dr. Eng. Allmi Syarif.

NIP. 196701031992031003

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NIP 197005012000031001

Nama . Dr. Eng. Suryadiwansa Harun

E-mail suryadiwansa.harun@eng.unila.ac.id

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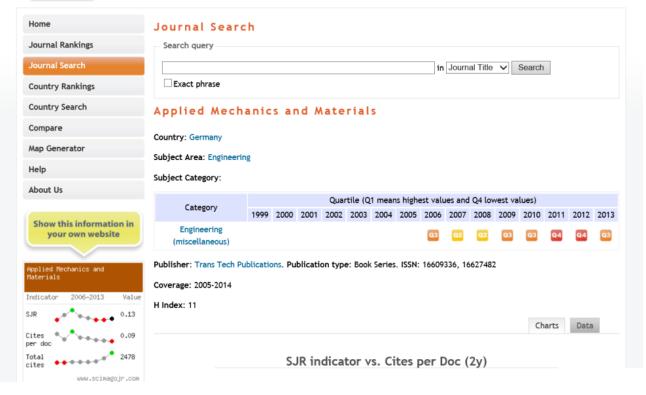
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FEM Simulation of Machining AISI 1045 Steel Using Driven Rotary Tool

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Yanuar Burhanuddin, Suryadiwansa Harun, Gusri Akhyar Ibrahim
Department of Mechanical Engineering, University of Lampung, Lampung – Indonesia
Email: yanuar.burhanuddin@eng.unila.ac.id

Keyword: driven rotary tool, tool rotational speed, force, temperature

Abstract. This study investigates the influences of driven rotary tool (DRT) on temperatures and forces when turning AISI 1045 steel. A set of cutting conditions was used in FE simulations to predict cutting force, stresses and temperatures developed at around the edge of tool. The material cutting speed ranges were set between 20 and 250 m min⁻¹. The rotary tool speed were 0 and 100 rpm. The feed rate and the depth of cut were set constant. Simulation results provided the predicted cutting distribution of temperatures and stresses at the chip and work piece.

Introduction

Machining of high strength steel using conventional cutting is very difficult and time consuming. During machining takes place, temperature and pressure will arise, this will lead to hardening due to the deformation or phase change of the materials. Therefore, instead of using conventional cutting cutting tool, machining of high-strength steel using a driven rotary tool may provide a better solution.

Rotary tool turning is a cutting process in which the cutting edge of a round insert rotates its axis, so that a continously indexed cutting edge is fed into the cutting zone [1]. There are two types of rotaty tool, self-propelled rotary tool (SPRT) and driven rotary tool (DRT). The difference between these two types is an auxillary drive unit to rotate the driven tool [2]. In SPRT, tool rotates due to the rotation of the workpiece while the DRT, the tool rotates due to driver motor. Self-rotation of a knife during machining process appears under influence of friction forces which appear in the point of contact of tool flank surface and machined surface. In the case of when angle $\alpha=0^{\circ}$ then the knife during machining doesn't rotate but when angle $\alpha\neq0^{\circ}$, a substantial contribution to self-rotation of knife has friction of a moving chip on the rake face [3].

In the rotary cutting tool, round inserts mounted on the tool holder will spin when engagement of the workpiece and the cutting tool. Because the rotary movement of the tool, the wear and heat will be distributed uniformly around the inserts. Uniform distribution of heat and wear at the cutting zone between the inserts and the workpiece will keep the temperature at an acceptable level. Thus hardening deformation or phase transformation can be avoided [1].

To obtain the characteristics of the rotary machining process, researchers require a lot of machining experiments. The vast machining experiments require a lot of cost and time. This gives an idea to the researchers to use finite element analysis. Investigators prefer the finite element analysis compared the experimental work because it can save time and costs [4].

Research of machining process simulation using rotary cutting tool is very rare. Until now none of literature on researches of rotary tool machining is reported. Most of the machining simulation researches are non-rotary tool machining simulation. There are many unknown phenomena in the rotary tool machining such as temperature distribution, tool wear, tool/workpice stress and workpiece surface integrity. In this study a finite element is applied to simulate AISI 1045 steel machining using rotary tool. The aim of this study is to determine temperature distribution in the work-piece, tool and chip and cutting force in turning process. The model is based on unsteady state machining condistion. AISI 1045 steel were turned under various cutting conditions. Various cutting conditions are cutting speed, feed rate, depth of cut and tool rotational speed.

Finite Element Modeling

The first step in finite element simulation of rotary tool machining is to establish the tool geometry. This geometry model including rake angle, relief angle and tool diameter as shown in Fig 1. The next step is to establish the finite element model of rotary tool turning. The finite element model of rotary tool is made based on the kinematic model of rotary turning. Kinematic and finite element model of rotary tool turning were illustrated in Fig 2a & b.

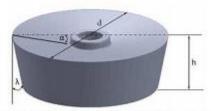


Fig 1. Tool geometry model (d=tool diameter, h=tool thickness, α=rake angle, λ=clearance angle)

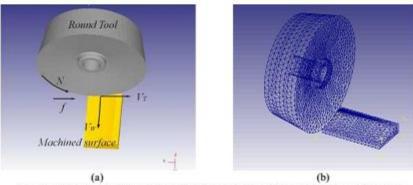


Figure 2 (a) Kinematic modeling of rotary tool, (b) Meshing of rotary tool turning

Finite element software was used to simulate the metal cutting process. It is based on the Updated Lagrangian formulation. This software is used to simulate machining parameters in a turning process of AISI 1045 carbon steel. Workpiece was assumed as plastic, whereas the tool was assumed as a rigid. The transfer of heat was taken into account to the modeling of cutting temperature.

Simulation process was done by varying the cutting speed, feed, depth of cut and tool rotation speed. The machining parameters is shown in Table I, while the type and geometry of material and tool are shown in Table 2.

Table 1. Machining parameters	s in simulation
Tool rotary speed N, Rpm	0~3000
Workpiece cutting speed VW, m/min	60 ~160
Feed, mm/rev	0.1;0.2
Depth of cut a, mm	0.5
Inclination angle, deg	00
Offset angle θ, deg	0

Table 2. Materia	type and cutting tool geometry	
Workpiece		
Material type	Plain Carbon Steel (AISI 1045)	
Material dimension	Diameter 50 mm	
Round Tool Insert		
	Uncoated tungsten carbide, WC-	
Material	Co	
	Jenis RPMT 1604 MO-BB	
Geometry	(Kyocera)	
Relief angle	α=11°C	
Diameter	D=16 mm	

Table 2. Material type and cutting tool geometry

The results of force and temperature on tool and workpiece would be analyzed. The initial temperature of the workpiece and the tool was set to 20 °C. Simulation was carried out until achieved a steady state condition to allow the flow of heat into the workpiece, tool and chip. Results and values observed on the tool and workpiece would be taken into account after the complete simulation.

Result and Discussion

The results from the turning process simulation using rotary cutting tool were analyzed after the complete simulation. There are two aspects to be analyzed namely cutting temperature and cutting force. Of the total energy consumed in machining, nearly all of it (approximately 99%) is converted into heat [5]. The heat was distributed between three areas namely tool, workpiece and chip during the machining process. A significant proportion of the cutting energy is carried off with the chip hence the chip temperature usually higher than two other areas. The temperature distribution on the interface of the tool-workpiece is illustrated in Fig 3a. While the temperature distribution on the chip where the largest temperature observed in this area is shown in Fig 3.b.

The results of the tool rotational speed effect on the machining temperature and cutting force are shown in Table 3 and Table 4. Table 3 contains the effect of tool rotational speed on the toolworkpiece interface temperature and chip temperature. Table 4 contains the effect of tool rotational speed on the main cutting force. In both tables it can be seen that the temperature and cutting force at lowest value when machining at tool rotational speed of 35 m/min. Therefore based on the value of tool cutting speed 35 m/min, the prediction of the effect of workpiece cutting speed on the cutting force and chip temperature will be simulated.

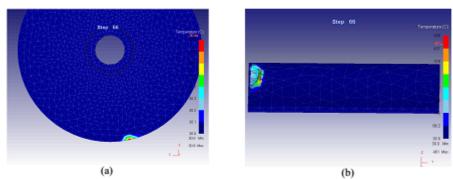


Fig. 3 (a) temperature distribution on the interface of the tool-workpiece, (b) temperature distribution on the chip

Table 3 The effect of tool rotary speed variation to tool-workpiece interface and chip temperature (Machining condition: V_w =150 m/min, f=0.2 mm/rev, a = 1 mm, i = 0,

 $\theta = 0$, and dry)

No. To all actions and distributions and distrib				
No	Tool rotation speed		Cutting tempe	
	N, Rpm	VT, m/min	Tool-workpiece	Chip, *C
			interface, C	
1.	0	0	432	787
2.	50	2.5	384	755
3.	100	5.0	377	724
4.	200	10	371	708
5.	300	15	392	716
6.	500	25	389	711
7.	650	32.5	347	752
8.	700	35	332	737
9.	750	37.5	324	689
10.	800	40	371	742
11.	900	45	375	754
12.	1000	50	378	751
13.	1500	75	408	758
14.	2000	100	419	775
15.	2500	125	414	794
16.	3000	150	546	1070

Table 4 The effect of workpiece cutting speed variation to main cutting force (Machining condition: V_w =80 m/min, f=0.2 mm/rev, a = 0.5 mm, i = 0, θ = 0, and dry)

No	Tool rotation speed		Main cuuting force Fy,
	N, Rpm	VT, m/min	N
1.	0	0	340,832
2.	100	5.0	367,820
3.	200	10	348,427
4.	300	15	364,161

continued..

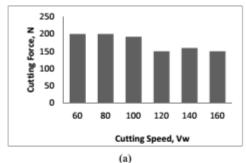
5.	500	25	354,084
6.	600	30	300,202
7.	700	35	281,639
8.	800	40	284,986
9.	1000	50	290,242
10.	1500	75	283,339
11.	2000	100	272,194
12.	2500	125	226,195
13.	3000	150	232,926

Table 5 and Fig. 4 show the result of workpiece cutting speed variation to main cutting force and chip temperature on the following machining condition: V_T =35 m/min, f=0.1 mm/rev, a = 0.5 mm, inclination angle = 0, θ = 0, and dry. At the cutting tool speed of 35 m/min, the cutting force and cutting temperature decrease with the increasing of cutting speed. The cutting force decrease from 200 N to 150 N. Decrease in cutting forces according to experiments conducted by Lei & Liu

[6]Decrease in cutting forces can be understood as the effect of thermal softening and reduced friction due to the increase in cutting speed. Thermal softening causes a decrease in strength of materials, the increase in friction angle and lower large plastic deformation [7]. But in this simulation cutting temperature decreases with increase in cutting speed. This is somewhat different from the usual obtained by other researchers. However, this temperature decrease is expected when going very rotating cutting tool wear in machining. Thus using a rotating cutting tool rotating at a speed of 35 m/min can be used.

Table 5 The effect of workpiece cutting speed variation to main cutting force and chip temperature (Machining condition: $V_T=35$ m/min, f=0.1 mm/rev, a=0.5 mm, i=0, $\theta=0$, and dry)

condition: v ₁ -33 hammi, 1-0.1 himatev, a - 0.3 him, 1 - 0, 0 -					
No	Workpiece cutting speed Vw, m/min	Cutting force, N	Cutting temperature (chip), °C		
1.	60	200	581		
2.	80	200	575		
3.	100	192	512		
4.	120	150	540		
5.	140	160	500		
6.	160	150	520		



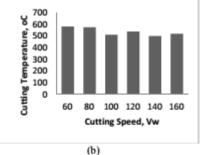


Fig. 4 (a) Effect of cutting speed on cutting forces, (b) Effect of cutting speed on chip temperature

Conclusions

The conclusions of this work can be drawn as follows:

- The cutting force and cutting temperature are in lowest value at the tool rotary of speed of 35 m/min.
- The cutting force and cutting temperature will decrease with the cutting speed increasing at tool speed of 35 m/min. Hence, to lower the temperature of the machining at high speed using driven rotary tool, the recommended tool rotational speed is 35 m/min.

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