# Effect of Sand Faction Percentage in Soil Mixture towards Soil Support Power for Dam Construction

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**Submission date:** 28-Jan-2022 01:29AM (UTC+0700)

**Submission ID:** 1749419641

File name: Power\_for\_Dam\_Construction\_Lusmeilia\_Afriani\_Ryzal\_Perdana.docx (215.55K)

Word count: 6259

Character count: 32679



#### 1 Research Article

#### 2 Effect of Sand Faction Percentage in Soil Mixture towards Soil

#### 3 Support Power for Dam Construction

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#### 8 Abstract

- 9 Knowledge of soil, which is an essential construction material, has a reat importance for dam
- 10 construction. The level of density and carrying capacity of the soil is very important for
- 11 consideration in the planning and designing stages of civil construction, considering the soil
- 12 functions as a n<sub>10</sub> ns to withstand the load or structure built on it. Stabilization using sand soil
- material is one of the ways to megathe strength requirements of soil carrying capacity when
- 14 there is no suitable soil material found in the nearby area. This paper aims to elucidate the
- physical properties of clay using a mixture of fine sand to reduce the risk of shrinkage when
- used for dam construction. Several analyses were undertaken to find out the effect of the fine
- sand percentage in the clay mixture to decrease the swelling test value and permeability test of the soil carrying capacity for dam construction. The types of soil tested were silt clays taken
- from Tritisan sub-district of East Lampung which was then stabilized using fine sand material
- from Central Lampung, Indonesia. This research was conducted using a mixture of sand, with
- a percentage of 10%, 20%, 30%, and 40%. Subgrade tests such as CBR, permeability tests
- were also undertaken to investigate other soil properties from each sample. The results in gicate
- 23 that a higher percentage of sand causes decreasing water content. Thus, the value of the
- 24 carrying capacity of the soil is increasing. The findings can be used to facilitate the increasing
- 25 use of clay mixtures with the percentage of fine sand in case suitable clay material cannot be
- 26 found around dam construction sites. The implications with suggestions for future research are
- 27 also discussed.
- 28 Keywords: sand fraction, soil mixture, construction

#### 29 Introduction

- 30 Knowledge of soil, which is a basic construction material, has great importance for dam
- 31 construction. It becomes the key factor of civilizations (Albaladejo, Diaz-Pereira, and De
- 32 Vente, 2020). In the history of geology, there is a close relationship between life and water
- from the per 172 ctive of the land and aquatic environment (Kocheeva, Roldugin, Katz, and
- Manankova,  $\overline{2019}$ ). The soil is the critical element of life support systems because it delivers
- 35 several ecosystem goods and services (Neina, 2019). Soil properties diverse considerably under
- 36 tillage type, intensity, different crops, fertilizer and application rates (Haruna & Nkongolo,
- 37 2013). It is well known that dam is one of irrigation infrastructure buildings with a type of weir



- structure that is affected by the fluctuating flow rates and water volumes of the river. Soil water 38 39 evaporation curves both represent the laws of water content variation in the natural state (Lei, 40 Liu, and Zhu, 2021). It constructs vital environmental protection and water management (Cui, Tian, Yang, Wen, and Khan, 2020). The occurrence of instability and the derailment of dam 41 construction can occur when the strength of the structure is not in accordance with shear 42 43 strength of the soil on the related site. It also gives nutrients on the sediments of the reservoir 44 (Zhang, Liao, Pei, Lu, Xu., and Wang, 2019). Besides the above things, however, many factors 45 can cause failures and cracks in a dam body such as floods, earthquakes or explosions, human 46 activities, and terrorist attacks against the dam (Poudel, Abbey, and Ngambi, 2017). Since dam 47 is a part of geotechnical engineering in civil engineering, if a failure occurs that finally causes 48 damage, it can be repaired by analyzing and designing the stability of the dam, including the 49 factors that affect the stability of the dam (Behzad Kalantari and Farjad Nazeri, 2016). It is 50 closely related to the decrease of taxa downstream and uplifts the biomass (Wu et al., 2019).
- In dam planning, it is generally accepted that one of the surveys that must be carried out is a material investigation (Dam Safety Center, 2003). One of the ways is by assessing the problems of dam constructions, which are built on clay in Indonesia and clay soil is spread almost in all areas of Indonesia. Regarding the dam construction, the original compacted soil is usually used as a core. In contrast, clay soil material is needed because it is impermeable so that the dam can store water to serve a function as a reservoir. Therefore, it leads to decreased upstream and downstream considerably (Jiang, Lu, Moran, Calvi, Dutra., and Li, 2018).

#### Soil Stabilization

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- Generally, soil stabilization refers to a particular way of improving soil properties through blending and mixing other materials. These improvements include the increasing dry unit weight, bearing capabilities, volume changes, the performance of *in situ* subsoils, sands, and other waste materials to strengthen road surfaces and other geotechnical applications (Firoozi et al., 2017). According to Bowles (1984), if the soil found in a site is loose or very easily stressed, or if it has an inappropriate consistency index, it has very high permeability or other undesirable traits that are not suitable for a development project. Soil stabilization must be carried out to resolve the above issues. In general, the method used to stabilize soil consists of one or a combination of the following processes (Bowles, 1984):
  - Mechanical, namely compaction with various types of mechanical equipment such as a roller machine, dropping heavy objects, explosion, static pressure, texture, freezing, heating and so on;
  - b. 20 ditive, namely the addition of gravel to cohesive soils, loam for grained so 20 and chemical mixers such as cement, lime, volcanic ash/coal, lime and/or cement, asphalt cement, sodium, and calcium chloride, paper mill waste, and others.
- The methods or ways to improve soil properties are also very dependent on curing time; this is because, during the process of improving soil properties, chemical processes occur, which require time for chemicals to present in the additive to react.
- However, the carrying capacity of the clay is often criticized for its low capacity. Clay soil is generally a poor subgrade due to its low shear strength, so that the construction of a structure on this soil layer always faces several problems such as low bearing capacity and large shrinkage properties. Therefore, it is commonly suggested that optimal water content plays an important role in getting the maximum density level. In addition to impermeability needs,

- 82 because a large number of soil volumes are needed, the source of the material is also one of the
- 83 important things to take into account.
- 84 Thus, the properties of clay are still not completely understood. In other words, evidence on
- 85 this question is presently inconclusive. Therefore, this paper aims to elucidate the physical
- 86 properties of this type of soil using a mixture of fine sand to reduce the risk of shrinkage when
- 87 used for dam construction.

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Soil is a collection of minerals, organic matter, and relatively loose deposits, which are located on bedrock (Hardrock) (Hardiyatmo, 1999). It is a collection of solid parts that are not bound to one another (some of which may be organic material) and the cavities between the parts containing air and water (Verhoef, 1994). According to Bowles (1984), soil is a mixture of particles consisting of one or all of the following types:

- a. Boulders are large pieces of rock, usually larger than 250 to 300 mm and ranging from of 150 mm to 250 mm in size; these rock fragments are called cobbles/pebbles;
- b. Gravel is a rock particle measuring 5 from mm to 150 mm;
- c. Sand is a rock particle measuring from 0.074 mm to 5 mm, which ranges from coarse with a size of 3 mm to 5 mm to fine material measuring <1 mm;
- d. Silt is rock particles measuring from 0.002 mm to 0.0074 mm;
- e. Clays are mineral particles smaller than 0.005 mm which are the main source of cohesion in cohesive soils;
- f. Colloids are mineral particles that are stationary and smaller than 0.001 mm.

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Several soil physical and biological properties, e.g., bulk density, aggregate stability and soil microbial biomass are related to the content and turnover of soil organic matter (SOM). Organic matter and clay are intimately linked by a range of physical, chemical and biological processes, playing a crucial role in the formation of soil aggregates, affecting stability at tolernt scales (Totsche et al., 2018).

- 109 Clay soils, which are very hard soil types in a dry state, are plastic at moderate water levels,
- whereas in higher water conditions, the clay will be sticky (cohesive) and very soft (Terzaghi
- 111 and Peck, 1987). It is the main concrete influencing dam safety operation (Fu, Su, and Wen,
- 112 2020). The clay fraction of silica by 59% can result in crystallinity and stability of temperature
- 113 (Charai, Sghiouri, Mezrhab, Karkri., and Hammouti, 2020). It mostly contains palygorskite,
- kaolin, and sepiolite minerals (Wang, Wang, Huang, and Tang, 2020). They can be used to
- 115 purify water and industrial substances (Ihekweme et al., 2020). The properties possessed by
- clay are as follows (Hardiyatmo, 1999):
- a. Fine-grain size, which is less than 0.002 mm;
- 118 b. Low permeability;
- 119 c. High capillary water rise:
- 120 d. Very cohesive:
- 121 e. High levels of shrinkage;
- 122 f. The process of consolidation is slow.
- Soft clay soil is soil containing clay minerals and has a high-water content, which causes low
- shear strength. Soft clay, also known as expansive clay, is a type of clay that is classified into
- 125 types of soil that have a development value and a large shrinkage value, so that it can cause
- damage to the structures built on it. Due to the amount of activity value (A) of clay soil, the
- 127 size of clay activity value is influenced by the soil plasticity index value (PI). Potential

- development of a type of soil is based on its plasticity index value (PI). Colay soils that can be
- 129 categorized into expansive clay soils are those having very high development potential limits
- 130 with the plasticity index value (PI) of > 35% (Charai, Sghiouri, Mezrhab, Karkri., and
- 131 Hammouti, 2020).
- Thus, the properties of clay are still no completely understood. In other words, evidence on
- this question is presently inconclusive. Sand is a naturally occurring granular material. Because
- of its high load bearing capacity in confined condition, sand could be used as a filler material.
- 135 It could be used in varying proportions as admixture to cohesive soils altering the properties of
- 136 plasticity, compaction and strength of the mixtures. Therefore, this paper aims to elucidate the
- physical properties of this type of soil using a mixture of fine sand to reduce the risk of
- shrinkage when used for dam construction.

#### Materials and Methods

#### 140 Research Sites

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- 141 This study focused on soil samples taken from Pringsewu and Margatiga Sub-districts in East
- Lampung Regency, Indonesia where dam construction was taking place.

#### 143 Soil Compaction

- 144 Compaction is an attempt to increase the density of the soil by releasing air to the soil porous,
- 145 which is usually done using mechanical energy. In the field, compaction effort is related to the
- amount of runoff from a roller machine, or something else that has the same principle for a
- 147 certain volume of soil. In general, soil compaction, which is carried out in the laboratory,
- 148 consists of two types, namely the AASHTO T 99 Proctor Standard (ASTM D 689) and
- 149 Modified Proctor, to obtain a greater California Bearing Ratio (CBR) value. Undertaking a soil
- 150 compaction test will make a connection between water content and volume weight. According
- to Bowles (1984), the benefits derived from compaction of soil include:
- a. Reduced subsidence, i.e., vertical movement within the soil mass itself due to reduced number of pores;
- b. Increasing soil strength;
- 155 c. Decreasing volume due to reduced water content during drying

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#### 156 California Bearing Ratio (CBR)

- 157 California Bearing Ratio (CBR), which was first invented between 19221930 in California by
- 158 O.J. Porter, is an empirical method for measuring soil density values. This method combines
- 159 an experiment of loading in the laboratory or in the field with an empirical plan to determine
- the thickness of the payement layer. A CBR test must first be carried out to get the CBR value.
- This test, a comparison between test loads with standard load and expressed as a percent, was
- developed around the 1930s in the laboratory of the Materials Research Department of the
- 163 California Division of Highway, USA

#### 164 **Dam Construction**

- 165 According to Indonesian Government Regulation Number 37 Article 1 of 2010 about Dams, a
- dam is a building made of earth, rock, concrete, and/or stone pairs to hold and store water. This
- is also built to hold and accommodate mine waste (tailings) or collect mud to form a reservoir.

A dam serves to function as a water catcher and saves the water during the rainy season when the river water flows in large quantities and exceeds the needs either for use, irrigation, drinking water, industry, or others. In the Guidelines and General Criteria of Dam Design (2003), the type of dam based on its function can be divided into:

- a. water reservoir dam;
- b. diversion dam:
- c. flood control dam;
- d. Multipurpose dam.

176 Based on the material, dams are classified into:

- concrete gravity dam;
- b. concrete dam with buttresses;
- 179 c. arch dam;

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- d. landfill dam;
- e. rockfill dams.

During the planning and designing stage, site selection and type of dam must be considered very carefully. The factors that should be taken into account when selecting the type of dam are as follows:

- a. The purpose of the dam building;
- b. Protection against overflow;
- c. Limitations on building expenses;
- d. Problems encountered in flow diversion during construction;
- e. Easy access to dam locations;
  - f. Availability of labor and equipment;
  - g. Physical factors of dam location;
  - h. Dam safely.

In other words, it is important to conduct surveys and investigations to determine the type and design of a a methat will be built. This is to avoid construction failure that can cause disaster. During the construction stage, several dam safety issues could be encountered, particularly the risk of piping failure of the existing dam due to foundation excavation for the dam construction. The variability in geology site, foundation conditions, construction materials, and site conditions of the project added to the risk of the project (Khor and Shamsuddin, 2019).

The material investigation must be carried out to assess and determine the physical and mechanical properties of the dam material and the availability of material reserves. The backfill dam material test is carried out to investigate the physical properties, dynamic properties, and rock tests. The test is carried out on waterproof material, semi-waterproof material, and watergraduated material. The need for this type of test is listed in the Guidelines, General Criteria, and Design of Dams (2003) for design and construction of reservoirs.

#### Sampling

The soil was sampled using a 4-inch tube with a length of 50 cm from three different locations. The tube was inserted into the ground at a depth of 50 cm. Plastic covers were used as soon as the earthen tube was removed to maintain its original moisture content. Soil samples were then taken to the lappratory for basic tests to obtain the basic properties that were later used as primary data, as shown in Figure 1 and Figure 2.

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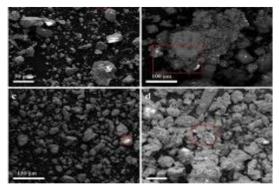
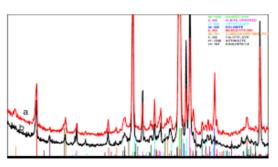


Figure 1. A soil sample from 3 different locations

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Figure 2. Soil XRD Findings

#### Equipment

The equipment used in this study were tools for filter analysis test (to assess for information and apply logic to get patterns of the study), specific gravity test (to see the concentration of all present particles), water content test (divide the mass of water by dry soil mass multiplied by 100), consistency limit test (control and identify small quantities of impurity in the substance), modified Proctor test (compaction of soil by its types and properties according to the change of moisture content, dry density and its relation), CBR test which belongs to a penetration test applied to evaluate road and pavement's strength. Its results are used by the curve to find out the layers' thickness of pavement and its component for flexible design (a cylindrical steel mold and by using a cylindrical steel plunger to force it with nominal diameter of 50 mm at a controlled rate), and other equipment to test the thickness of layers (Atterberg Limits, Calcium Carbonate Content, Expansion and Swell of Soil) in the Soil Mechanical Laboratory, Department of Civi 40 ngineering, University of Lampung, which has been 18 itable with the standardization of the American Society for Testing Materials (ASTM) by D698 or AASHTO T99 and modified ASTM D1557 and AASHTO T180. To test the soil mixture, three tests were applied including; permeability test (to know the ability of porous media), compaction test (to identify soil compaction properties), and pinhole test (to find out clay soils dispersity).

#### Method of Mixing Soil and Sand Samples

- This research was conducted using sand as a mixture with variations in the percentage of sand of 10%, 20%, 30%, and 40% (ASTM International, 2015).
- 240 Data Processing and Analysis

- 241 Basic soil tests such as water content, soil content, Atterberg limit, compaction, permeability,
- 242 swelling, and triaxial were undertaken at the Soil Mechanical Laborat of the Department of
- 243 Civil Engineering, the University of Lampung following ASTM by D698 or AASHTO T99
- 244 and modified ASTM D1557 and AASHTO T180. The ASTM Standard is used to develop and
- 245 publish voluntary consensus of technical standard for various products, materials, services, and
- 246 system (ASTM International, 2015).

#### **Permeability Test**

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248 Permeability illustrates the ability of porous media, which allows fluid to flow. The flow of

- 249 water through granular soil or rock mass is a common concern in geotechnical engineering. It
- 250 is defined as the movement of fluid by porous media linked with materials' durability (Wang,
- 251 Liu, Feng, et al., 2016). The samples were tested using a fiting head procedure with the
- 252 coefficient of permeability (k) as the output. This experiment is a common laboratory testing
- 253 method used to determine the permeability of fine-grained soils with intermediate and low
- 254 permeability such as silts and clays. The falling head permeability test involves the flow of
- 255 water through a relatively short soil sample connected to a standpipe, which provides the water
- 256 head, which also allows measuring the vol 12 e of water passing through the sample. Firstly,
- 257 saturated and standpipes soil samples were filled with de-aired water to a given level. The test
- 258 was then started by allowing water to by through the soil sample until it reached a given
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- lower limit. The time received for the water to drop from the upper to the lower level was 260
- 27 orded. The steps were repeated for a couple of times in which the recorded times should be
- 261 within an allowable variation of about 10% otherwise, the test was considered as a failure. The
- 262 method was used to look at the coefficient of permeability.

#### **Compaction Test**



- A standard proctor compaction test was undertaken to find out the soil compaction properties 264
- 265 where it has the optimal water content at which soil can reach its maximum dry density. It
- 266 recognized and established guidelines to provide criteria for performance and methodologies
- 267 test for compaction (ASTM International, 2015). The output of this test would then be used to
- 268 make CBR test samples. Samples were soaked for four days to see the changes of volume, and
- 269 a dial gauge was installed to measure the volume changes. Shrinkage value could be read from
- 270 the swelling value measured by the dial gauge.

#### Pinhole Test

- 272 A pinhole test was conducted to investigate the dispersity of clay soils. The piping failures of
- 273 a number of homogeneous earth dams, erosion along channel or canal banks, and rainfall
- 274 erosion of earthen structures have been attributed to the colloidal erosion along cracks or other
- 275 flow channels formed in masses of dispersive clay from Tritisan sub-district of East Lampung,
- 276 Indonesia. The test was undertaken by flowing water horizontally with 50 mm of air pressure
- 277 on soil samples, and a hole was made with 1 mm of diameter. It was firstly proposed as a tool
- 278 to evaluate susceptibility of compacted fine-grained soils to pipping by using a flow of passing
- 279 water (Sherard et al, 1976). Also, the pinhole test, Emerson crumb test, was conjucted.
- 280 Emerson's crumb test provided the potential of clay soils erodibility by using ASTM D4647 /
- 281 D4647M - 13(2020) as the Standard Test Methods for Identification and Classification of
- 282 Dispersive Clay Soils by the Pinhole Test. The test consisted of a cubical specimen of about
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- 15 mm on a sidoor selecting an air-dried soil crumb of about equal volume. The specimen was
- 284 then placed in distilled water. As the soil began to hydrate, the tendency for colloidal-sized
- 285 particles to deflocculated and suspend was observed.

#### **Results and Discussion**

Preliminary research, including soil properties testing, soil physical properties, and compaction testing was conducted. The data obtained in this study came from a series of filter analysis tests carried out in the laboratory, then presented systematically and clearly so that it could be analyzed. The data obtained were specific gravity, liquid limit and plastic limit, MDD, OMC, UCS, and CBR values without curing and UCS and curing CBR. From the results of the preliminary survey, dam body materials could be obtained from the surrounding area in terms of volume. The physical properties themselves did not meet the technical requirements for a dam Biochemical Oxygen Demand (BOD) although the soil material from surrounding area could be used as the mixture of fine sand. The analysis results of soil samples taken from the study sites conducted in the laboratory can be seen in Table 1.

Table 1. Soil sample testing result

No	Sample	Depth	Density			Triaxial UU					
	Code		MDD	OMC	MBD	Joule	С	W	Density	Gs	
		(m)	(Kn/m <sup>3</sup> )	(%)	(Kn/m <sup>3</sup> )	(degree)	(kPa)	%	(Kn/m <sup>3)</sup>		
1	26	01.40	1.190	37.16	1.632	13.50	1.61	31.94	1.62	2.57	
2	AL.6	01.00-01.40	1.190	47.28	1.753	16.02	1.23	44.76	1.58	2.56	
3	AL.7	01.40	1.160	38.09	1.602	20.92	0.37	37.99	1.59	2.59	
4	AL.7	02.30	1.160	39.58	1.619	16.20	1.29	37.33	1.68	2.57	
5	AL.8	01.50	1.280	39.85	1.790	16.14	1.32	36.37	1.69	2.58	
6	AL.8	02.60	1.250	37.27	1.716	10.13	2.24	38.08	1.74	2.60	
7	AL.9	01.30	1.200	39.46	1.674	10.07	1.45	39.81	1.68	2.65	
8	$\frac{1}{22}$ .9	02.60	1.250	47.52	1.844	19.02	1.11	39.21	1.64	2.55	
9	TP.1	02.00	1.310	38.39	1.813	12.21	1.01	35.22	1.67	2.51	
10	TP.1-1	01.00-01.40	1.330	35.35	1.800	17.34	0.37	35.98	1.70	2.64	
11	TP.2-1	01.00-01.40	1.250	35.47	1.693	15.77	0.82	34.52	1.71	2.64	
12	TP.4	01.00-01.40	1.390	32.20	1.838	6.11	1.07	32.89	1.73	2.44	
13	TP.4-2	02.10	1.320	35.78	1.792	17.87	0.30	32.24	1.70	2.54	
14	TP.8	01.75-02.15	1.350	43.88	1.942	4.26	0.56	48.36	1.71	2.55	
15	TP.9	01.30-01.70	1.130	44.44	1.632	14.64	0.82	49.24	1.65	2.44	
16	TP.11	02.60-03.00	1.420	32.20	1.877	13.80	0.94	43.44	1.73	2.42	
17	TP.11-1	01.60-02.00	1.070	41.17	1.510	25.40	0.22	40.95	1.60	2.48	

In expansive soil, such as clay, it is acceptable to state that the volume of soil changes related to the change of water content and its pessure occurred in the soil. These volume changes can lead to either swelling or shrinkage. The pressure, which the expansive soil exerts if it is not allowed to swell or the volume change of the soil drained, is known as swelling pressure of soil. The swelling pressure is affected by several factors such as (a) the type of clay in the soil and the nature of clay minerals; (b) moisture content and dry density; (c) fluid properties; (d) soil stress and pressure limits; and (e) drying and wetting cycle. After the CBR and shear strength (qu) values were obtained for each variation of clay and sand from the study sites, the CBR and qu values were analyzed in relation to influential factors such as soil mix

composition, soil density, and also water content. It needs to be seen that the CBR value and the shear strength value (qu) are related to the soil mixture that an increase in shear strength and CBR occurs significantly after mixing sand gradation into the clay (Al Hafizh, Wibisono, Nugroho, 2017). The following are the results of the analysis of soil properties, as shown in Table 2.

Table 2. Indexes Properties of Soil

integers no. 200	egers				φ	γ	$S_r$		$C_c$			PΙ
	integers no. 4	(cm/s)	%	(kPa)	(°)	(gr/cm³)	. Sr	(cm²/s)		%	%	%
13.66	58.72	2.80.E- 03	31.94	0.68	14.79	1.19	76.15	0.34	0.47	53.45	41.21	12.24
6.25	77.21	8.13.E- 03	44.76	0.41	20.20	1.19	102.93	0.38	0.12	68.17	55.45	12.71
19.71	66.31	3.11.E- 04	37.99	0.30	30.26	1.16	79.82	0.26	0.14	58.88	48.95	9.93
11.56	70.56	1.98.E- 02	37.33	0.35	30.05	1.16	81.13	0.30	0.05	60.86	43.36	17.50
9.37	68.56	1.46.E- 02	36.37	0.28	29.32	1.28	89.43	0.31	0.13	61.08	46.72	14.36
17.27	63.82	9.37.E- 04	38.08	0.34	30.76	1.25	98.23	0.48	0.24	46.36	31.07	15.29
19.70	67.05	1.11.E- 03	39.81	0.32	29.54	1.20	104.40	0.20	0.05	72.85	58.00	14.85
14.21	70.05	1.40.E- 03	39.21	0.31	33.69	1.25	89.28	0.48	0.36	64.75	47.52	17.23
19.45	54.68	3.29.E- 03	35.22	0.31	27.62	1.31	101.37	0.94	0.07	62.95	51.37	11.58
8.12	77.18	6.88.E- 03	35.98	0.25	32.01	1.33	95.52	0.43	0.11	56.45	42.90	13.54
20.04	65.01	4.26.E- 04	34.52	0.22	22.62	1.25	83.04	0.35	80.0	51.95	41.79	10.16
15.02	73.74	2.14.E- 03	32.89	0.31	23.67	1.39	104.73	0.35	0.11	44.56	25.78	18.78
16.78	50.84	1.49.E- 03	32.24	0.33	25.56	1.32	93.39	0.46	0.14	58.31	35.17	23.14
6.90	71.89	8.84.E- 03	48.36	0.70	16.08	1.35	129.74	0.37	0.10	71.36	53.74	17.62
14.10	71.14	1.89.E- 03	39.24	0.35	28.74	1.13	97.43	0.16	0.07	64.64	51.37	13.27
14.33	48.95	2.51.E- 03	43.44	0.37	21.06	1.42	123.80	0.36	0.29	73.49	51.19	22.30
19.85	66.24	2.46.E- 04	40.95	0.35	27.99	1.07	77.21	0.24	0.10	64.91	52.44	12.47
	6.25 19.71 11.56 9.37 17.27 19.70 14.21 19.45 8.12 20.04 15.02 16.78 6.90 14.10 14.33	6.25 77.21  19.71 66.31  11.56 70.56  9.37 68.56  17.27 63.82  19.70 67.05  14.21 70.05  19.45 54.68  8.12 77.18  20.04 65.01  15.02 73.74  16.78 50.84  6.90 71.89  14.10 71.14  14.33 48.95	13.66     38.72       19.71     66.31       19.71     66.31       3.11.E-04       11.56     70.56       1.98.E-02       9.37     68.56       1.46.E-02       17.27     63.82       19.70     67.05       1.11.E-03       14.21     70.05       1.40.E-03       19.45     54.68       3.29.E-03       8.12     77.18       6.88.E-03       20.04     65.01       4.26.E-04       15.02     73.74       2.14.E-03       16.78     50.84       1.49.E-03       14.10     71.14       1.89.E-03       14.33     48.95       2.51.E-03       19.85     66.24       2.46.E-1	13.66       58.72       03       31.94         6.25       77.21       8.13.E- 03       44.76         19.71       66.31       3.11.E- 04       37.99         11.56       70.56       1.98.E- 02       37.33         9.37       68.56       1.46.E- 02       36.37         17.27       63.82       9.37.E- 04       38.08         19.70       67.05       1.11.E- 03       39.81         14.21       70.05       1.40.E- 03       39.21         19.45       54.68       3.29.E- 03       35.22         8.12       77.18       6.88.E- 03       35.98         20.04       65.01       4.26.E- 04       34.52         15.02       73.74       2.14.E- 03       32.89         16.78       50.84       1.49.E- 03       32.24         6.90       71.89       8.84.E- 03       48.36         14.10       71.14       1.89.E- 03       39.24         14.33       48.95       2.51.E- 03       43.44         19.85       66.24       2.46.E- 40.95	13.66       58.72       03       31.94       0.68         6.25       77.21       8.13.E- 03       44.76       0.41         19.71       66.31       3.11.E- 04       37.99       0.30         11.56       70.56       1.98.E- 02       37.33       0.35         9.37       68.56       1.46.E- 02       36.37       0.28         17.27       63.82       9.37.E- 04       38.08       0.34         19.70       67.05       1.11.E- 03       39.81       0.32         14.21       70.05       1.40.E- 03       39.21       0.31         19.45       54.68       3.29.E- 03       35.22       0.31         8.12       77.18       6.88.E- 03       35.98       0.25         20.04       65.01       4.26.E- 03       34.52       0.22         15.02       73.74       2.14.E- 03       32.89       0.31         16.78       50.84       1.49.E- 03       32.24       0.33         6.90       71.89       8.84.E- 03       48.36       0.70         14.10       71.14       1.89.E- 03       39.24       0.35         14.33       48.95       2.51.E- 03       43.44       0.37 <td>13.66       58.72       03       31.94       0.68       14.79         6.25       77.21       8.13.E- 04       44.76       0.41       20.20         19.71       66.31       3.11.E- 04       37.99       0.30       30.26         11.56       70.56       1.98.E- 02       37.33       0.35       30.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32         17.27       63.82       9.37.E- 04       38.08       0.34       30.76         19.70       67.05       1.11.E- 03       39.81       0.32       29.54         14.21       70.05       1.40.E- 03       39.21       0.31       33.69         19.45       54.68       3.29.E- 03       35.98       0.25       32.01         20.04       65.01       4.26.E- 04       34.52       0.22       22.62         15.02       73.74       2.14.E- 03       32.89       0.31       23.67         16.78       50.84       1.49.E- 03       32.24       0.33       25.56         6.90       71.89       8.84.E- 03       48.36       0.70       16.08         14.10       71.14       <td< td=""><td>13.66       38.72       03       31.94       0.68       14.79       1.19         6.25       77.21       8.13.E- 03       44.76       0.41       20.20       1.19         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33         8.12       77.18       6.88.E- 03       35.98       0.25       32.01       1.33         20.04       65.01       4.26.E- 04       34.52       0.22       22.62       1.25         15.02       73.74       2.14.E- 03       32.89       0.31       23.67</td><td>13.66       58.72       03       31.94       0.88       14.79       1.19       76.15         6.25       77.21       8.13.E-       03       44.76       0.41       20.20       1.19       102.93         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82         11.56       70.56       1.98.E-       02       37.33       0.35       30.05       1.16       81.13         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43         17.27       63.82       9.37.E-       38.08       0.34       30.76       1.25       98.23         19.70       67.05       1.11.E-       39.81       0.32       29.54       1.20       104.40         14.21       70.05       1.40.E-       39.21       0.31       33.69       1.25       89.28         19.45       54.68       32.9.E-       35.22       0.31       27.62       1.31       101.37         8.12       77.18       68.8.E-       35.98       0.25       32.01       1.33       95.52         20.04       65.01       4.26.E-       34.52</td><td>13.66       58.72       03       31.94       0.68       14.79       1.19       76.15       0.34         6.25       77.21       8.13.E-       03       0.41       20.20       1.19       102.93       0.38         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82       0.26         11.56       70.56       1.98.E-       37.33       0.35       30.05       1.16       81.13       0.30         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43       0.31         17.27       63.82       9.37.E-       04       38.08       0.34       30.76       1.25       98.23       0.48         19.70       67.05       1.11.E-       03       39.81       0.32       29.54       1.20       104.40       0.20         14.21       70.05       1.40.E-       03       39.21       0.31       33.69       1.25       89.28       0.48         19.45       54.68       3.29.E-       03       35.22       0.31       27.62       1.31       101.37       0.94         8.12       77.18       6.88.E-<td>13.66       38.72       03       31.94       0.08       14.79       1.19       76.15       0.34       0.47         6.25       77.21       8.13.E- 04       44.76       0.41       20.20       1.19       102.93       0.38       0.12         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16       79.82       0.26       0.14         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16       81.13       0.30       0.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28       89.43       0.31       0.13         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25       98.23       0.48       0.24         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20       104.40       0.20       0.05         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25       89.28       0.48       0.36         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33       9</td><td>13.66         58.72         03         31.94         0.68         14.79         1.19         76.15         0.34         0.47         53.45           6.25         77.21         8.13.E- 03         44.76         0.41         20.20         1.19         102.93         0.38         0.12         68.17           19.71         66.31         3.11.E- 04         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88           11.56         70.56         1.98.E- 02         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86           9.37         68.56         1.46.E- 02         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08           19.70         67.05         0.31-E- 02         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36           19.70         67.05         0.31-M.E- 03         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75           19.45         54.68         3.29.E- 03         35.22         0.31</td><td>13.66         58.72         03         31.94         0.88         14.79         1.19         76.15         0.34         0.47         53.45         41.21           6.25         77.21         8.13.E-         0.34         0.41         20.20         1.19         102.93         0.38         0.12         68.17         55.45           19.71         66.31         3.11.E-         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88         48.95           11.56         70.56         1.98.E-         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86         43.36           9.37         68.56         1.46.E-         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08         46.72           17.27         63.82         9.37.E-         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36         31.07           19.70         67.05         1.40.E-         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75         47.52</td></td></td<></td>	13.66       58.72       03       31.94       0.68       14.79         6.25       77.21       8.13.E- 04       44.76       0.41       20.20         19.71       66.31       3.11.E- 04       37.99       0.30       30.26         11.56       70.56       1.98.E- 02       37.33       0.35       30.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32         17.27       63.82       9.37.E- 04       38.08       0.34       30.76         19.70       67.05       1.11.E- 03       39.81       0.32       29.54         14.21       70.05       1.40.E- 03       39.21       0.31       33.69         19.45       54.68       3.29.E- 03       35.98       0.25       32.01         20.04       65.01       4.26.E- 04       34.52       0.22       22.62         15.02       73.74       2.14.E- 03       32.89       0.31       23.67         16.78       50.84       1.49.E- 03       32.24       0.33       25.56         6.90       71.89       8.84.E- 03       48.36       0.70       16.08         14.10       71.14 <td< td=""><td>13.66       38.72       03       31.94       0.68       14.79       1.19         6.25       77.21       8.13.E- 03       44.76       0.41       20.20       1.19         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33         8.12       77.18       6.88.E- 03       35.98       0.25       32.01       1.33         20.04       65.01       4.26.E- 04       34.52       0.22       22.62       1.25         15.02       73.74       2.14.E- 03       32.89       0.31       23.67</td><td>13.66       58.72       03       31.94       0.88       14.79       1.19       76.15         6.25       77.21       8.13.E-       03       44.76       0.41       20.20       1.19       102.93         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82         11.56       70.56       1.98.E-       02       37.33       0.35       30.05       1.16       81.13         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43         17.27       63.82       9.37.E-       38.08       0.34       30.76       1.25       98.23         19.70       67.05       1.11.E-       39.81       0.32       29.54       1.20       104.40         14.21       70.05       1.40.E-       39.21       0.31       33.69       1.25       89.28         19.45       54.68       32.9.E-       35.22       0.31       27.62       1.31       101.37         8.12       77.18       68.8.E-       35.98       0.25       32.01       1.33       95.52         20.04       65.01       4.26.E-       34.52</td><td>13.66       58.72       03       31.94       0.68       14.79       1.19       76.15       0.34         6.25       77.21       8.13.E-       03       0.41       20.20       1.19       102.93       0.38         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82       0.26         11.56       70.56       1.98.E-       37.33       0.35       30.05       1.16       81.13       0.30         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43       0.31         17.27       63.82       9.37.E-       04       38.08       0.34       30.76       1.25       98.23       0.48         19.70       67.05       1.11.E-       03       39.81       0.32       29.54       1.20       104.40       0.20         14.21       70.05       1.40.E-       03       39.21       0.31       33.69       1.25       89.28       0.48         19.45       54.68       3.29.E-       03       35.22       0.31       27.62       1.31       101.37       0.94         8.12       77.18       6.88.E-<td>13.66       38.72       03       31.94       0.08       14.79       1.19       76.15       0.34       0.47         6.25       77.21       8.13.E- 04       44.76       0.41       20.20       1.19       102.93       0.38       0.12         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16       79.82       0.26       0.14         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16       81.13       0.30       0.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28       89.43       0.31       0.13         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25       98.23       0.48       0.24         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20       104.40       0.20       0.05         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25       89.28       0.48       0.36         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33       9</td><td>13.66         58.72         03         31.94         0.68         14.79         1.19         76.15         0.34         0.47         53.45           6.25         77.21         8.13.E- 03         44.76         0.41         20.20         1.19         102.93         0.38         0.12         68.17           19.71         66.31         3.11.E- 04         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88           11.56         70.56         1.98.E- 02         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86           9.37         68.56         1.46.E- 02         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08           19.70         67.05         0.31-E- 02         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36           19.70         67.05         0.31-M.E- 03         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75           19.45         54.68         3.29.E- 03         35.22         0.31</td><td>13.66         58.72         03         31.94         0.88         14.79         1.19         76.15         0.34         0.47         53.45         41.21           6.25         77.21         8.13.E-         0.34         0.41         20.20         1.19         102.93         0.38         0.12         68.17         55.45           19.71         66.31         3.11.E-         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88         48.95           11.56         70.56         1.98.E-         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86         43.36           9.37         68.56         1.46.E-         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08         46.72           17.27         63.82         9.37.E-         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36         31.07           19.70         67.05         1.40.E-         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75         47.52</td></td></td<>	13.66       38.72       03       31.94       0.68       14.79       1.19         6.25       77.21       8.13.E- 03       44.76       0.41       20.20       1.19         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33         8.12       77.18       6.88.E- 03       35.98       0.25       32.01       1.33         20.04       65.01       4.26.E- 04       34.52       0.22       22.62       1.25         15.02       73.74       2.14.E- 03       32.89       0.31       23.67	13.66       58.72       03       31.94       0.88       14.79       1.19       76.15         6.25       77.21       8.13.E-       03       44.76       0.41       20.20       1.19       102.93         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82         11.56       70.56       1.98.E-       02       37.33       0.35       30.05       1.16       81.13         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43         17.27       63.82       9.37.E-       38.08       0.34       30.76       1.25       98.23         19.70       67.05       1.11.E-       39.81       0.32       29.54       1.20       104.40         14.21       70.05       1.40.E-       39.21       0.31       33.69       1.25       89.28         19.45       54.68       32.9.E-       35.22       0.31       27.62       1.31       101.37         8.12       77.18       68.8.E-       35.98       0.25       32.01       1.33       95.52         20.04       65.01       4.26.E-       34.52	13.66       58.72       03       31.94       0.68       14.79       1.19       76.15       0.34         6.25       77.21       8.13.E-       03       0.41       20.20       1.19       102.93       0.38         19.71       66.31       3.11.E-       04       37.99       0.30       30.26       1.16       79.82       0.26         11.56       70.56       1.98.E-       37.33       0.35       30.05       1.16       81.13       0.30         9.37       68.56       1.46.E-       02       36.37       0.28       29.32       1.28       89.43       0.31         17.27       63.82       9.37.E-       04       38.08       0.34       30.76       1.25       98.23       0.48         19.70       67.05       1.11.E-       03       39.81       0.32       29.54       1.20       104.40       0.20         14.21       70.05       1.40.E-       03       39.21       0.31       33.69       1.25       89.28       0.48         19.45       54.68       3.29.E-       03       35.22       0.31       27.62       1.31       101.37       0.94         8.12       77.18       6.88.E- <td>13.66       38.72       03       31.94       0.08       14.79       1.19       76.15       0.34       0.47         6.25       77.21       8.13.E- 04       44.76       0.41       20.20       1.19       102.93       0.38       0.12         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16       79.82       0.26       0.14         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16       81.13       0.30       0.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28       89.43       0.31       0.13         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25       98.23       0.48       0.24         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20       104.40       0.20       0.05         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25       89.28       0.48       0.36         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33       9</td> <td>13.66         58.72         03         31.94         0.68         14.79         1.19         76.15         0.34         0.47         53.45           6.25         77.21         8.13.E- 03         44.76         0.41         20.20         1.19         102.93         0.38         0.12         68.17           19.71         66.31         3.11.E- 04         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88           11.56         70.56         1.98.E- 02         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86           9.37         68.56         1.46.E- 02         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08           19.70         67.05         0.31-E- 02         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36           19.70         67.05         0.31-M.E- 03         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75           19.45         54.68         3.29.E- 03         35.22         0.31</td> <td>13.66         58.72         03         31.94         0.88         14.79         1.19         76.15         0.34         0.47         53.45         41.21           6.25         77.21         8.13.E-         0.34         0.41         20.20         1.19         102.93         0.38         0.12         68.17         55.45           19.71         66.31         3.11.E-         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88         48.95           11.56         70.56         1.98.E-         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86         43.36           9.37         68.56         1.46.E-         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08         46.72           17.27         63.82         9.37.E-         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36         31.07           19.70         67.05         1.40.E-         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75         47.52</td>	13.66       38.72       03       31.94       0.08       14.79       1.19       76.15       0.34       0.47         6.25       77.21       8.13.E- 04       44.76       0.41       20.20       1.19       102.93       0.38       0.12         19.71       66.31       3.11.E- 04       37.99       0.30       30.26       1.16       79.82       0.26       0.14         11.56       70.56       1.98.E- 02       37.33       0.35       30.05       1.16       81.13       0.30       0.05         9.37       68.56       1.46.E- 02       36.37       0.28       29.32       1.28       89.43       0.31       0.13         17.27       63.82       9.37.E- 04       38.08       0.34       30.76       1.25       98.23       0.48       0.24         19.70       67.05       1.11.E- 03       39.81       0.32       29.54       1.20       104.40       0.20       0.05         14.21       70.05       1.40.E- 03       39.21       0.31       33.69       1.25       89.28       0.48       0.36         19.45       54.68       3.29.E- 03       35.98       0.25       32.01       1.33       9	13.66         58.72         03         31.94         0.68         14.79         1.19         76.15         0.34         0.47         53.45           6.25         77.21         8.13.E- 03         44.76         0.41         20.20         1.19         102.93         0.38         0.12         68.17           19.71         66.31         3.11.E- 04      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8.13.E-         0.34         0.41         20.20         1.19         102.93         0.38         0.12         68.17         55.45           19.71         66.31         3.11.E-         37.99         0.30         30.26         1.16         79.82         0.26         0.14         58.88         48.95           11.56         70.56         1.98.E-         37.33         0.35         30.05         1.16         81.13         0.30         0.05         60.86         43.36           9.37         68.56         1.46.E-         36.37         0.28         29.32         1.28         89.43         0.31         0.13         61.08         46.72           17.27         63.82         9.37.E-         38.08         0.34         30.76         1.25         98.23         0.48         0.24         46.36         31.07           19.70         67.05         1.40.E-         39.21         0.31         33.69         1.25         89.28         0.48         0.36         64.75         47.52

Compressibility is an important parameter in a dam construction due to its instability that might cause bigger problems such as collapsing. The experiments showed that the coefficient of consolidation (Cv) obtained was in the range of 0.201 cm²/sec to 0.942 cm²/sec with 29.44% and 34% of sand that passed sieve no. 200 and no.4, respectively. Meanwhile, the values of the compression index (Cc) obtained were between 0.48 to 0.29, as seen in Table 1. The most significant consolidation occurred when the ratio of the fine grain was much higher than clay, is showed by the high value of Cv. It presents essential environmental protection and water management (Cui, Tian, Yang, Wen, and Khan, 2020). However, the compressibility process might happen during and after the construction process as newly added loads. At this rate, it might become very extensive and excessive pore water pressure.

#### Relationship between water content with frictional angle, cohesion, and density

The presence of water content creates pore water pressure that affects the effective str25 of soil. In addition to water content, soil cohesion, shear strength, and compaction energy affect the bearing capacity of the soil. The relationship between water content, frictional angels, cohesion, and density is shown in Figure 3.

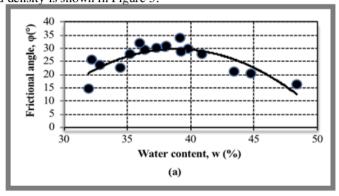


Figure 3. Highest cohesion value

Figure 3 shows the relationship between water content and frictional angle. The result shows that the frictional angle value increased as the water content increased until it reache 360% of water content. The frictional angle value was obtained from the Triaxial CU test. Figure 3 illustrates the relationship between soil cohesion and water content. The result shows that the cohesion decreased rapidly with increasing water content and did not change much afterward.

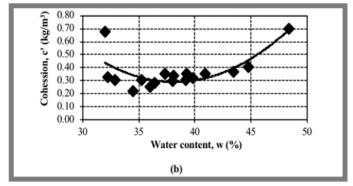
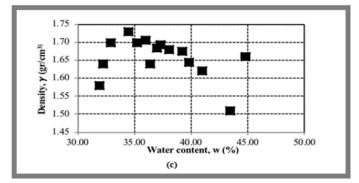


Figure 4. Highest cohesion value-added water

Figure 4 gives information about the relationship between water content and soil density. The result shows that the maximum density was obtained with 32% of optimum water content, and it kept decreasing as water content increased. The frictional angle is closely related to the cohesion of soil. The frictional angle and cohesion of soil are increased to a maximum value along with the addition of water content. The highest cohesion value was obtained when water was added in its optimum volume, which was between 37% and 40%, as seen in Figure 3 and Figure 4. There were 17 experiments carried out in total. However, 2 experiments showed dissimilar results. At water content between 35% and 40%, the soil density ranged from 1.15 gr/m³ to 1.35 gr/m³ and decreased with further water addition, as seen in Figure 5. It is line with the decreasing upstream and downstream considerably between content and soil density (Jiang, Lu, Moran, Calvi, Dutra., and Li, 2018).



#### Figure 5. Decreased water addition

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#### The Relationship between Soil Mixture Variations and Permeability

It was found from the experiments that he clay and sand ratio affected the coefficient of permeability. The result showed that the coefficient of permeability decreased correspondingly with the increment of clay ratio. Meanwhile, the coefficient of permeability reached 10-7 when the clay content was 41%. This result does not fit the requirements of soil that can be used as filter material, which allows less than 5% of clay contained in the material where the clay will be sticky (cohesive) and very soft (Terzaghi and Peck, 1987). However, the soil from the surrounding area may still be used as body dam material with proper compaction, as referred to in SNI 8062: 2015 (Earth-fill Dam Regulation). The relationship between clay and sand ratio in soil with respect to the coefficient of permeability is shown in Figures 6 and 7 below.

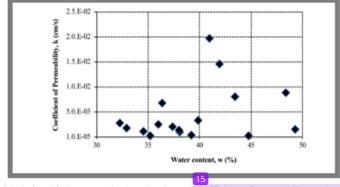
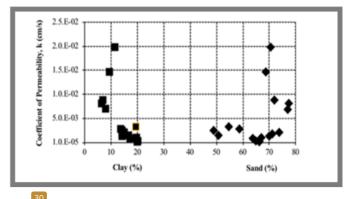


Figure 6 Relationship between clay/sand ratio and coefficient of permeability and water content



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Figure 7 Relationship between the coefficient of permeability and water content

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#### Relationship between Water Content and Permeability

The value of the coefficient of permeability is also related to water content. The experiment was conducted with water content ranging between 32% and 49%, which was insignificant indifference. The value of the permeability coefficient obtained was between  $2.4 \times 10^{-4}$  and  $1.4 \times 10^{-2}$ , as seen in Figure 4. As a result, it is judicious to say that the sand/clay ratio affected the coefficient of permeability (k) more than the water content. This study also examined the dispersion degree of clay through visual examination, Emerson crumb test, and pinhole test. The results of the Emerson crumb test showed that all samples could be categorized as Grade 1, which means that no colloidal cloud developed. Even though the crumb may slake and particles spread away from the original cloud because of this slaking activity, no trace of a colloidal cloud was observed in the chloride solution affecting the stability of the dam (Behzad Kalantari and Farjad Nazeri, 2016).

#### Conclusions

Based on the results of data analysises and processing, the soil stabilization for the dams using silt clay from Pringsewu and Margatiga sub-districts in East 24 npung Regency, Indonesia is as follows: An increase in the value of the figure angle is caused by an increase in water content up to 40%; A decrease in cohesion is caused by an increase in water content and does not change much afterward; The optimum density value occurs when the water content is 32%. The higher the moisture content, the lower the density; The highest cohesion value is obtained when water is added in its optimum volume which is between 37% and 40%; Soil density values range from 1.15 g/m<sup>3</sup> to 1.35 g/m<sup>3</sup> in which the water content is between 35% and 40%, g/m<sup>3</sup>. The increasing addition of water reduces the compressibility value; The ratio of clay and sand affects the coefficient of permeability. The results show that the permeability coefficient decreases with increasing clay ratio. With testing on water content ranging between 32% and 49%, the difference is not significant. Permeability coefficient values obtained are between  $2.4 \cdot 10^{-4}$  and  $1.4 \cdot 10^{-2}$ . This press that the sand/soil ratio affects the permeability coefficient (k) more than the water content. Based on the laboratory testings of the soil, the results do not suit the needs of the soil, which can be used as a filter, which allows less than 5% of the clay contained in the material. However, soils from the area around the dam construction site taking place in Pringsewu and Margatiga Sub-districts in East Lampung Regency can still be used as dam materials with proper compaction as referred to in SNI.

#### **Conflict of Interest Disclosure**

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The authors whose names are listed immediately in this paper certify that they have NO affiliations with or involvement in any organization or entity with any financial interest (such as honoraria; educational grants; participation in speakers' bureaus; membership, employment, consultancies, stock ownership, or other equity interest; and expert testimony or patent-licensing arrangements), or non-financial interest (such as personal or professional relationships, affiliations, knowledge or beliefs) in the subject matter or materials discussed in this manuscript.

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#### Acknowledgments

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- 418 This research was supported by the Research and Community Service Institution of Lampung
- 419 University, Indonesia through the research grant in 2020.

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